# **Robot Perception and Control** Kinematics and Control

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## **Kinematics**

### **Kinematics**

Kinematics: study of a motion of the robot without considering the forces and torques producing the motion.

### **Denavit–Hartenberg convention**

The following four transformation parameters are known as D–H parameters:

- $a_i$ : distance from  $z_{i-1}$  to  $z_i$  along  $x_i$ .
- $\alpha_i$ : angle from  $z_{i-1}$  to  $z_i$  about  $x_i$ .
- $d_i$ : distance from  $x_{i-1}$  to  $x_i$  along  $z_i$ .
- $\theta_i$ : angle from  $x_{i-1}$  to  $x_i$  about  $z_i$ .

Usually,  $a_i$  and  $\alpha_i$  are **constants** that describe the geometry of the robot, while  $d_i$  and  $\theta_i$  are the **variables** that describe the motion of prismatic and revolute joints, respectively.



### **Denavit–Hartenberg convention**

In this convention, coordinate frames are attached to the joints between two links such that one transformation is associated with the joint [Z], and the second is associated with the link [X]. The coordinate transformations [T] along a serial robot consisting of n links form the kinematics equations of the robot as:

 $[T] = [Z_1][X_1][Z_2][X_2]\dots[Z_n][X_n]$ 

where each transformation [Z][X] can be implemented as a  $4 \times 4$  matrix using the DH parameters as:

def transform(a, alpha, d, theta): return Rot(theta, axis="z") @ Trans(d, axis="z") @ Trans(a, axis="x") @ Rot(alpha, axis="x")

### **Forward Kinematics**

Forward kinematics is the problem of finding the end-effector position and orientation x(t) of a robot manipulator given the joint angles  $\theta(t)$  and link lengths.

x(t) = f( heta(t))

We can use the DH parameters of a robot to simply represent the forward kinematics as a chain of transformations starting from a **base link**, which connects to the origin.

```
def fk(theta):
    trans = np.identity(4)
    for (_a, _alpha, _d, _theta) in dh_params(theta):
        trans = trans @ transform(_a, _alpha, _d, _theta)
    return trans
```

### **Forward Kinematics**

Let's consider the *right front leg* joints (coordinate systems below):



11	ne DH	paran	neters of	the	leg:		
-	Link	a	lpha	d	θ		
_	0-1	$L_1$	0	0	$ heta_1$		
	1-2	0	$-\pi/2$	0	$-\pi/2$		
	2-3	$L_2$	0	0	$ heta_2$		
	3-4	$L_3$	0	0	$ heta_3$		
Fr	om th	e tab	le, we o	can	construct		
th	e each	trans	sformatio	on 7	and the		
fo	rward	kinen	natics is	giv	en by the		
ch	ain of	thos	e transf	orm	ations as		
$T_{(}$	4 )•						

	$\left[\cos(\theta_1)\right]$	$-\sin( heta_1)$		$0  -L_1\cos( heta_1)$			1
$T^1$ –	$\sin( heta_1)$	$\cos(t)$	$\cos( heta_1)$		$-L_1\sin( heta_1)$		
$I_{0} -$	0	0	0		0		ļ
		0		0	1		
	[	0	-1	0	0		
	$T^2$ –	-1	0	0	0		
	$\boldsymbol{r}_1 - \boldsymbol{r}_1$	0	0	1	0		
	l	0	0	0	1_		
	$\left[\cos(\theta_2)\right]$	$-\sin( heta_2)$		0	$L_2\cos( heta_2)^{-1}$		1
$T^3$ —	$\sin( heta_2)$	cos	$\cos( heta_2)$		$L_2\sin( heta_2)$		
$I_2 -$	0	(	0		0		
	0	0		0	1 .		
	$\left[\cos(\theta_3)\right]$	$-\sin$	$-\sin( heta_3)$		$L_3\cos( heta_3)$		1
$T^3$ —	$\sin( heta_3)$	$\cos$	$\cos( heta_3)$		$L_3\sin( heta_3)$		
$I_2 -$	0	(	0		0		
		(	0		1		
	$T_0^4$	$=T_{0}^{1}$	$T_{1}^{2}T_{1}^{2}$	$T_{2}^{3}T_{3}$	$\frac{4}{3}$		

### **Inverse Kinematics**

Inverse kinematics (IK) is essentially the reverse operation of FK: computing configuration(s) to reach a desired workspace coordinate. Unlike forward kinematics, inverse kinematics cannot be solved in a closed-form expression (in general). If we can derive a closed-form expression through symbolic manipulations, we can use Analytical IK, otherwise we need to use numerical approach.

#### **Analytical IK**

- Once the equations are derived, solutions are very fast to compute.
- Often difficult or tedious to derive.
- Only applicable to non-redundant robots (# DOFs = # of task space dimensions).

#### **Numerical IK**

- need to define solution parameters or initial guesses
- More generalizable

### **Analytical Inverse Kinematics**

Let's consider a 2D arm in 2D space as in the Figure. From law of cosines:

$$\cos(\pi- heta_2)=-rac{x_2^2+y_2^2-L_1^2-L_2^2}{2L_1L_2}$$

Assuming solution exists ( $-1 \le RHS \le 1$ ),

$$heta_2 = \pm \cos^{-1}\left(rac{x_2^2 + y_2^2 - L_1^2 - L_2^2}{2L_1L_2}
ight)$$

• Note that *elbow down* and *elbow up* solutions  $(\pm)$  exist.

Then using the  $\theta_2$ , we can find a  $\theta_1$  as:

$$heta_1 = atan 2(y_2,x_2) - atan 2(L_2\sin heta_2,L_1+L_2\cos heta_2)$$

### **Analytical Inverse Kinematics**

Given the foot position  $(x_4, y_4, z_4)$ , the joint positions  $\theta_1, \theta_2, \theta_3$  for a typical quadruped leg is given as in paper **f**:

$$egin{aligned} heta_1 &= - atan 2(-y_4, x_4) - atan 2\left(\sqrt{x_4^2 + y_4^2 - L_1^2}, -L_1
ight) \ heta_2 &= atan 2\left(z_4, \sqrt{x_4^2 + y_4^2 - L_1^2}
ight) - atan 2\left(L_3 \sin( heta_3), L_2 + L_3 \cos( heta_3)
ight) \ heta_3 &= atan 2\left(\pm \sqrt{1 - D^2}, D
ight) \end{aligned}$$

where

$$D=rac{x_4^2+y_4^2+z_4^2-L_1^2-L_2^2-L_3^2}{2L_2L_3}$$

• the  $\pm$  sign in  $\theta_3$  determines the knee direction if the quadruped.



### Jacobian

The Jacobian matrix is a matrix of partial derivatives that describes how the robot's configuration affects the robot's end-effector position. The Jacobian matrix is defined as:

$$J = \frac{\partial x}{\partial \theta}$$

where *x* is the end-effector position and  $\theta$  is the joint angles.

If we consider the differentiation w. r. t. time, we can write the relationship between  $\dot{x}$  (or v) and  $\dot{\theta}$ .

 $\dot{x} = J( heta) \dot{ heta} \ \dot{ heta} = J^{-1}( heta) \dot{x}$ 

### **Basic Jacobian**

### **Numerical Inverse Kinematics**

Given an initial guess  $\theta^0$  that is close to a solution  $\theta_d$ , the kinematics can be expressed as the Taylor expansion:

$$egin{aligned} x_d &= f( heta_d) = f( heta^0) + rac{\partial f}{\partial heta} \Big|_{ heta^0} ( heta_d - heta^0) + ext{h.o.t.} \ &= f( heta^0) + J( heta^0) \Delta heta + ext{h.o.t.} \end{aligned}$$

where  $J(\theta^0)$  is the coordinate Jacobian at  $\theta^0$ .

By truncating the Taylor expansion at first order, we can obtain the approximation as:

$$J( heta^0)\Delta heta=x_d-f( heta^0)$$

Assuming that  $J(\theta^0)$  is square and invertible, we can solve for  $\Delta \theta$  as:

$$\Delta heta = J^{-1}( heta^0)(x_d - f( heta^0))$$

• In practice, **pseudo-inverse** of a Jacobian  $J^+$  is used and we do not need to assume square and invertible.

We will **iteratively update** the guess until it converges to a solution.

$$heta^{i+1} \longleftarrow heta^i + \eta \Delta heta$$